## SDG&E, June 15, 2018 Rulemaking (R.) 15-01-008 to Adopt Rules and Procedures Governing Commission Regulated Natural Gas Pipelines and Facilities to Reduce Natural Gas Leaks Consistent with Senate Bill 1371, Leno. In Response to Data Request, R15-01-008 2018 June Report Appendix 9; Rev. 03/31/18

System Categories	Emission Source Categories	Emission Factor Sources	Description [in natural gas volume]	Explanatory Notes/Comments
	Transmission Pipeline Leaks	Engineering Estimate	Emissions estimated from size of breach / pressure / duration calculation	For 2017, the INGAA Greenhouse Gas Emission Estimation Guidelines for Natural Gas Transmission and Storage - Volume 1 GHG Emission Estimation Methodologies and Procedures (September 28, 2005 - Revision 2) - Table 4-4 study provides the best available estimate of emissions for Transmission Pipeline, which includes emissions from Flanges and Valves. The emissions for the component leaks reported in "Component leaks" worksheet are accounted for by this mileage-based INGAA Emission Factor.
	All damages (as defined by PHMSA)	Engineering Estimate	Emissions estimated either from modelling or size of breach / pressure / duration	
	Transmission Pipeline Blowdowns	Engineering Estimate	Unique equipment volume (corrected for pressure and temperature)	For the Transmission Odor Intensity Test; Annual Emission = Number of Tests * Volume per Test
Transmission Pipeline	Pneumatic Devices - Pneumatic/Hydraulic Valve Operators, and Turbine Valve Operators	MRR	Low Continuous Bleed = 0.0336 Mscf/day/dev Intermittent Bleed = 0.0576 Mscf/day/dev High Continuous Bleed = 0.4457 Mscf/day/dev Hydraulic Valve Operator = TBD Turbine Valve Operator = TBD	
	Pressure Relief Valves	MRR	Pressure relief valve = 0.9713 Mscf/day/dev	
	Odorizer (Odorizer and Gas Sampling Vents)	TCR	1.27 Mscf/yr/odorizer (if manufacturing specs are available, use the manufacting specs instead of the default emission factor)	The following equations adhere to manufacturing specifications: For Transmission (BTU) Gas Chromatographs (GCs); Annual Emission = (Number of GCs * Sample Flow + Number of GC Streams * Bypass Flow) * Unit conversion factor. • For Transmission (Gas Quality) Gas Chromatographs (GCs); Annual Emission = (Number of GCs * Sample Flow + (Number of GCs + Number of Additional Streams) * Flow "Genie") * Unit conversion factor. • For Odorizer; Annual Emission = Number of strokes * Emission per stroke, where Number of strokes = (Gas Volume * Injection Rate)/(Odorant Density * Pump Stroke Volume) * Unit conversion factor.
	M&R Stations - Farm Taps & Direct Industrial Sales	MRR	<pre># of leaks &gt; 10,000 ppm x Subpart W EF (ref: Table W-3 of Subpart W of Part 98) Farm Tap / Direct Sale = 12.2 Mscf/yr/station Non-compressor components Valve = 0.1572 Mscf/day/dev Connector = 0.1399 Mscf/day/dev Open-ended line = 0.276 Mscf/day/dev Pressure relief valve = 0.0492 Mscf/day/dev Meter = 0.0728 Mscf/day/dev</pre>	
Transmission M&R	M&R Stations - Transmission-to-Transmission Company Interconnect	MRR	# of leaks > 10,000 ppm x Subpart W EF (ref: Table W-3 of Subpart W of Part 98) Trans-to-trans = 1,554.8 Mscf/yr/station <b>Non-compressor components</b> Valve = 0.1572 Mscf/day/dev Connector = 0.1399 Mscf/day/dev Open-ended line = 0.276 Mscf/day/dev Pressure relief valve = 0.0492 Mscf/day/dev Meter = 0.0728 Mscf/day/dev	<ul> <li>The vented emissions for pneumatic devices reported in the "Component Vented Emissions" worksheet for Transmission M&amp;R Stations are accounted for as part of the station's emission factor, which is 1,554.8 Mscf/yr/station.</li> <li>The fugitive emissions for the component leaks reported in "Component Leaks" worksheet for Transmission M&amp;R Stations are accounted for as part of the station's emission factor, which is 1,554.8 Mscf/yr/station.</li> </ul>

System Categories	Emission Source Categories	<b>Emission Factor Sources</b>	Description [in natural gas volume]	Explanatory Notes/Comments
	Transmission M&R Leaks	MRR	# of leaks > 10,000 ppm x Subpart W EF (ref: Table W-3 of Subpart W of Part 98) Non-compressor components Valve = 0.1572 Mscf/day/dev Connector = 0.1399 Mscf/day/dev Open-ended line = 0.276 Mscf/day/dev Pressure relief valve = 0.0492 Mscf/day/dev Meter = 0.0728 Mscf/day/dev	
	Transmission M&R blowdown	Engineering Estimate	Unique equipment volume (corrected for pressure and temperature)	See Appendix 2 Explanatory Notes / Comments
Transmission Compressor Stations	Compressor station - Equipment leaks from valves, connectors, open ended lines, pressure relief valves, and meters (using leak detection)	MRR	# of leaks > 10,000 ppm x Subpart W EF (ref: Table W-3 of Subpart W of Part 98) Non-compressor components Valve = 0.1572 Mscf/day/dev Connector = 0.1399 Mscf/day/dev Open-ended line = 0.276 Mscf/day/dev Pressure relief valve = 0.0492 Mscf/day/dev Meter = 0.0728 Mscf/day/dev	<pre># of leaks &gt; 10,000 ppm x Subpart W EF (ref: Table W-3 of Subpart W of Part 98) Compressor components Valve = 0.35616 Mscf/day/dev Connector = 0.13416 Mscf/day/dev Open-ended line = 0.41448 Mscf/day/dev Pressure relief valve = 0.95184 Mscf/day/dev Meter = 0.46392 Mscf/day/dev</pre>
	Compressor Station - Transmission storage tanks	MRR	Direct measurement of tank vapor vent stack + operating hours (pg 218-219 of Regulation for MRR)	Annual Emissions for Tank Pressure Release Due to Temperature Fluctuation: The initial volume of gas released is calculated based on starting and ending pressures assuming a constant -260°F in the tank. This volume is then adjusted to standard conditions (scf). Note: Pressure normally fluctuates slightly in the main tank due to instrument measurement accuracy, but any drop in pressure 1 psi or greater is typically due to a fill or maintenance procedure (including the vapor releases to maintain a safe operating pressure). An hourly pressure read from the LNG SCADA data is downloaded and all pressure drops meeting the above criteria are captured.
	Compressors (Centrifugal) - Transmissiondata collection will require time spent in modes (active, pressurized idle, de-pressurized idle), compressor venting	MRR	Direct measurement x operating hours (operating mode)	
	Compressors (Reciprocating) - Transmissiondata collection will require time spent in modes (active, pressurized idle, de-pressurized idle)compressor rod packing venting	MRR	Direct measurement x operating hours (operating mode)	
	Compressor station - Equipment and pipeline blowdowns	MRR	Eq. W - 14A # of blowdowns * piping volume	LNG Tank annual emissions for Total Gas Lost Due to Filling Operations: The volume of gas delivered is recorded as gallons. This volume is then converted to standard conditions (scf).
	Compressor Station - Natual gas pneumatic device venting	MRR	Low Continuous Bleed = 0.0336 Mscf/day/dev Intermittent Bleed = 0.0576 Mscf/day/dev High Continuous Bleed = 0.4457 Mscf/day/dev	
	Distribution Mains (Below-Ground Leaks)	GRI (1996)	Unprotected Steel Main = 0.1548 Mscf/day/leak Protected Steel Main = 0.0612 Mscf/day/leak Plastic Main = 0.2988 Mscf/day/leak	
	Distribution Mains (Above Ground Leaks) - Not MSA	GRI (1996)	Unprotected Steel Main = 0.1548 Mscf/day/leak Protected Steel Main = 0.0612 Mscf/day/leak Plastic Main = 0.2988 Mscf/day/leak	
	Distribution Service (Below-Ground Leaks)	GRI (1996)	Copper = 0.0226 Mscf/day/leak Unprotected Steel Service = 0.0600 Mscf/day/leak Protected Steel Servce = 0.0276 Mscf/day/leak Plastic Service = 0.0089 Msc/day/leak	
	Distribution Service (Above-Ground Leaks) - Not MSA	GRI (1996)	Copper = 0.0226 Mscf/day/leak Unprotected Steel Service = 0.0600 Mscf/day/leak Protected Steel Servce = 0.0276 Mscf/day/leak Plastic Service = 0.0089 Msc/day/leak	
	Distribution Main, Pressure Relief Valves	MRR	Pressure relief valve = 0.00696 Mscf/day/dev	

System Categories	Emission Source Categories	Emission Factor Sources	Description [in natural gas volume]	Explanatory Notes/Comments
Distribution Mains and Services Pipelines	Distribution Mains and Services blowdown	MRR	Equation W-14A , Eq. W-35 , Eq. W-36	For an Abandoned High/Medium Pressure Pipe and Service; Annual Emission = pi * ((Pipe Diameter)^2)/4 * Blowdown Footage * Pressure conversion factor/Natural Gas Compressibility Factor. Note that for shut-in pressures less than 100 psig, the Natural Gas Compressibility Factor is 1. For the Distribution Odor Intensity Test; Annual Emission = Number of Tests * Volume per Test
	All damages (as defined by PHMSA)	MRR	Equation W-14A , Eq. W-35 , Eq. W-36	<ul> <li>For AG Non-hazardous and MSA damages, emissions were estimated based on a company emission factor for the maximum leak rate of AG Non-hazardous based on soap test criteria for above ground facilities: number of days leaking * 4 cfh * 24/1000 = Mcf/damage.</li> <li>For AG Hazardous and Below Ground Code 1 damages, emissions were estimated based on engineering calculations using pipe size, damage opening size, and duration. Where an estimate was not made at the time of the event, the emissions were estimated from a population of similar events with respect to pipe material and size.</li> <li>For Code 2 and Code 3 damages, the emission factor for Distribution pipeline leaks was used (line 24 and 26).</li> </ul>
	Pneumatic Devices - Pneumatic/Hydraulic Valve Operators, and Turbine Valve Operators	Engineering Estimate	Manufacturer Supplied Information (e.g., Bristol, Becker, Moore, etc)	
	Distribution Above grade M&R Station Leaks ( > 300 psi)	GRI (1996)	1,684.5 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
	Distribution Above grade M&R Station Leaks (100 - 300 psi)	GRI (1996)	896.5 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
	Distribution Above grade M&R Station Leaks ( < 100 psi)	GRI (1996)	40.6 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
Distribution M&R Stations	Distribution Below grade M&R Station Leaks (> 300 psi)	GRI (1996)	12.176 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
	Distribution Below grade M&R Station Leaks (100 - 300 psi)	GRI (1996)	1.840 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
	Distribution Below grade M&R Station Leaks (< 100 psi)	GRI (1996)	0.964 Mscf/yr/station	The fugitive emissions for the component leaks reported in the "Component Leaks" worksheet for Distribution M&R Stations are accounted for as part of the station's emission factor.
	Distribution M&R Station Blowdowns	Engineering Estimate	Average Pressure x Average Volume x # of inspections & Maintenance Activities	See Appendix 5 Explanatory Notes / Comments
	Distribution M&R Station Pneumatics	Engineering Estimate	Manufacturer Supplied Information (e.g., Bristol, Bettis Actuators, etc)	
	Residential Meters	GRI (1996)	0.148 Mscf/yr/meter	
	Commercial and Industrial Meters	GRI (1996)	0.051 Mscf/yr/meter	

System Categories	Emission Source Categories	Emission Factor Sources	Description [in natural gas volume]	Explanatory Notes/Comments
Commercial, Industrial and Residential Meters	All damages (as defined by PHMSA)			<ul> <li>For AG Non-hazardous MSA damages, emissions were estimated based on a company emission factor for the maximum leak rate of AG Non-hazardous leaks based on soap test criteria for above ground facilities: number of days leaking</li> <li>4 cfn * 24/1000 = Mcf/damage.</li> <li>For AG Hazardous MSA damages, emission was estimated based on engineering calculation using pipe size, damage opening size, and duration. Where an estimated from a population of similar events with respect to pipe material and pipe size.</li> </ul>
	Vented Emission from MSA	Engineering Estimate	Estimated volume release by MSA and activity type	See Appendix 6 Explanatory Notes / Comments
	Dehydrator Vents - Storage	GRI (1996)	One of the following three cases per dehydrator facility 1. Glycol dehydrator with VRU and thermal oxidizer = 0 Mscf	
			2. Glycol dehydrator with no control device = Engineering Estimate	
			3. Desiccant dehydrator = 2.23E-03 mt CH4/MMscf (Alternative: Eq. 5 in MRR)	
underground storage	Storage - piping leakage	MRR	Leaker EFsStorage Station, Gas Service (Survey was conducted, and only recorded leaking components use following EFs) Valve = 129.998 Mscf/yr/dev Connector = 49.573 Mscf/yr/dev Open-Ended Line = 151.285 Mscf/yr/dev Pressure Relief Valve = 347.422 Mscf/yr/dev Meter = 169.331 Mscf/yr/dev Population EFsStorage Wellheads, Gas Service (Survey was not conducted, all components use following EFs) Connector = 0.0876 Mscf/yr/dev Valve = 0.0876 Mscf/yr/dev Pressure relief Valve = 1.489 Mscf/yr/dev Open Ended Line = 0.2628 Mscf/yr/dev	
	Storage - surface casing leakage	Engineering Estimate	TBD	
	Storage - Wellhead leakage	Engineering Estimate	leak survey + extrapolation	
	Storage - Compressor & blowdowns	Engineering Estimate	Eq. 13 of MRR (piping volume x # of blowdowns)	
	Storage - Wellhead Rework blowdown and bring-in	Engineering Estimate	Eq. 9,10,11,12 of MRR	
	Pressure Relief Valves Pneumatic Devices - Pneumatic/Hydraulic Valve Operators, and Turbine Valve Operators	MRR	Pressure relief vallve = 0.9713 Mscf/day/dev. Low Continuous Bleed = 0.0336 Mscf/day/dev Intermittent Bleed = 0.0576 Mscf/day/dev High Continuous Bleed = 0.4457 Mscf/day/dev Hydraulic Valve Operator = TBD Turbine Valve Operator = TBD	